Journal of Power Sources 185 (2008) 895-898

Contents lists available at ScienceDirect

## Journal of Power Sources

journal homepage: www.elsevier.com/locate/jpowsour





# Effects of hydrazine addition on gas evolution and performance of the direct borohydride fuel cell

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#### ARTICLE INFO

Article history: Received 17 July 2008 Received in revised form 20 August 2008 Accepted 20 August 2008 Available online 27 August 2008

Keywords: Sodium borohydride Hydrazine Anodic oxidation Gas evolution Cell performance

#### ABSTRACT

A fuel cell configuration using alkaline NaBH<sub>4</sub>–N<sub>2</sub>H<sub>4</sub> solutions as the fuel is suggested. Gas evolution behaviors and cell performances of alkaline NaBH<sub>4</sub>–N<sub>2</sub>H<sub>4</sub> solutions on different catalysts have been studied. It is found that gas evolution behaviors are influenced by the applied anodic catalysts and the concentration of NaBH<sub>4</sub> and N<sub>2</sub>H<sub>4</sub>. NaBH<sub>4</sub> is mainly electro-oxidized on Pd but N<sub>2</sub>H<sub>4</sub> is mainly electro-oxidized on Ni and surface-treated Zr–Ni alloy when using NaBH<sub>4</sub>–N<sub>2</sub>H<sub>4</sub> solutions as the fuel and a composite of Pd, Ni and surface-treated Zr–Ni alloy as the anodic catalyst. The cyclic voltammetry results show that electrochemical oxidation potential of NaBH<sub>4</sub> is higher than that of N<sub>2</sub>H<sub>4</sub>. Adding hydrazine into alkaline sodium borohydride solutions can suppress gas evolution and improve the cell performance of the DBFC. The performances of fuel cells using NaBH<sub>4</sub>–N<sub>2</sub>H<sub>4</sub> solutions are comparable to that of fuel cell using N<sub>2</sub>H<sub>4</sub> solution.

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#### 1. Introduction

Compared with the direct methanol fuel cell (DMFC), the direct borohydride fuel cell (DBFC) demonstrates high electromotive force (emf) of 1.64 V and high capacity of  $5.67 \text{ Ah g}^{-1}$  [1–5].

Theoretically, one BH<sub>4</sub><sup>-</sup> can generate eight electrons through following anodic reaction:

$$BH_4^- + 8OH^- \to BO_2^- + 6H_2O + 8e^-$$
(1)

However, in practical, the generated electrons are usually less than eight. In general, the anodic oxidation of  $BH_4^-$  can be described as [6,7]:

$$BH_4^- + xOH^- \to BO_2^- + (x-2)H_2O + (4-1/2x)H_2 + xe^-$$
(2)

Here, x represents the actual number of the electrons released by each  $BH_4^-$  and it is called coulumbic number in following paragraphs. The coulumbic number depends on applied anode catalyst and fuel composition.

Many studies have been carried out aiming at clarifying the anodic oxidation mechanism of  $BH_4^-$  at many catalysts [8–15]. The anodic reaction of  $BH_4^-$  on Ni electrode is a 4e reaction (corresponding to x=4) [6,10,11]. Liu reported a 4e reaction of  $BH_4^-$  occurred on AB<sub>2</sub> or AB<sub>5</sub> hydrogen storage alloys when using

high concentrated borohydride solutions [12,13]. Higher coulumbic number can be achieved at Pd/C or Pt/C electrode when using borohydride solutions with relatively low concentrations [7,11,14]. Gyenge et al. reported that Pt–Ni and Pt–Ir exhibited higher electrocatalytic activity than Pt [15]. Adding a carbon supported Pd into the Ni anode not only depressed the hydrogen evolution but also improved the DBFC performance [16]. Therefore, a composite catalyst prepared by mixing Ni, Pd/C and surface-treated Zr–Ni alloy was used as anode catalyst in this work.

The hydrogen evolution occurs during operation if the coulumbic number is less than 8, which results in decreasing of the fuel utilization and the cell performance. How to restrain hydrogen evolution is one of the critical issues in the development of the DBFC technology [5,16]. It is considered that hydrogen evolution could be suppressed by optimizing fuel composition through adding some components that could inhibit hydrogen generation. Gyenge reported that thiourea was an effective inhibitor of the catalytic hydrolysis associated with BH<sub>4</sub><sup>-</sup> electro-oxidation on Pt [17]. The BH<sub>4</sub><sup>-</sup> utilization efficiency and coulombic efficiency of DBFC were improved by adding thiourea into the alkaline NaBH<sub>4</sub> solutions.

It is considered that hydrazine  $(N_2H_4)$  is alkalescent and could stabilize borohydride because borohydrides are stable only in alkaline media. Furthermore,  $N_2H_4$  itself can be used as a fuel in the direct hydrazine fuel cell (DHFC) [21]. In this work, we tried to add  $N_2H_4$  into the alkaline NaBH<sub>4</sub> solution to stabilize BH<sub>4</sub><sup>-</sup> and to improve the cell performance. The cell performance and gas evo-

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**Fig. 1.** Gas evolution rates of alkaline  $NaBH_4-N_2H_4$  solutions on the catalyst composite of Pd/C, Ni and surface-treated Zr–Ni alloy. NaOH concentration: 10 wt.%.

lution behavior were investigated and the functions of the  $N_2 H_4$  addition were discussed.

#### 2. Experimental details

Anode electrodes were prepared by brushed anode catalyst paste into a piece of Ni foam with a catalyst loading of 10 mg cm<sup>-2</sup>. The paste was composed of Nafion solution (5 wt.%) and anode catalysts. We tested the hydrogen evolution at Ni powder (INCO 210), surface-treated Zr-Ni alloy [19], Pd/C (10% Pd on Vulcan XC-72, E-Tek Co.) and their composite catalyst during operation. The composite catalyst was prepared by mixing Ni powder, surfacetreated Zr-Ni allov and Pd/C with a mass ratio of 0.75:0.75:0.6. Cathodes were commercially available with a catalyst loading of Pt 1 mg cm<sup>-2</sup> (Pt 30 wt.% on Vulcan XC-72, E-Tek Co.). Nafion N117 membrane was used to separate cathode and anode. The flow field area of end plates was 6 cm<sup>2</sup>. The test cell structure was described in our previous paper [9]. Alkaline NaBH<sub>4</sub> and N<sub>2</sub>H<sub>4</sub> solutions containing 10 wt.% of NaOH were used as the fuel. Polarizations of the alkaline NaBH<sub>4</sub> and N<sub>2</sub>H<sub>4</sub> solutions were determined by cyclic volatammetry (CV) measurement. Cell performances were measured at a fuel flow rate of 10 ml min<sup>-1</sup> and an oxygen flow rate of 0.15 L min<sup>-1</sup> at ambient conditions. The amount of generated gas from the anode was determined by water displacement method.

The gas evolution rates of alkaline  $NaBH_4$  and  $N_2H_4$  solutions on Ni, Pd, surface-treated Zr–Ni alloy and composite catalyst were measured in a three-electrode system as described in our previous paper [7]. All experiments were performed at ambient conditions.

#### 3. Results and discussion

#### 3.1. Gas evolution

One of the critical disadvantages of the DBFC is the hydrogen evolution during operation because hydrogen evolution will significantly reduce fuel efficiency and lower the cell performance [20]. It has been reported that  $N_2H_4$  could be electro-oxidized by following reaction [21]:

$$N_2H_4 + 40H^- \rightarrow N_2 + 4H_2O + 4e^-$$
 (3)

The gas evolution rates of the 4e reaction of NaBH<sub>4</sub> and the 4e reaction of N<sub>2</sub>H<sub>4</sub> are given in Fig. 1. We studied the effect of N<sub>2</sub>H<sub>4</sub> addition on the gas evolution behavior on the composite cat-



Fig. 2. Gas evolution rates of alkaline NaBH\_4-N\_2H\_4 solutions on the Pd/C catalyst. NaOH concentration: 10 wt.%.

alyst of Ni, Pd and surface-treated Zr–Ni alloy when using alkaline  $NaBH_4-N_2H_4$  solutions.

As shown in Fig. 1, it can be seen that the gas evolution rate of the alkaline N<sub>2</sub>H<sub>4</sub> solution agreed well with the stoichiometric relation of the 4e reaction of N<sub>2</sub>H<sub>4</sub> according to Eq. (3). However, alkaline NaBH<sub>4</sub>-N<sub>2</sub>H<sub>4</sub> solutions demonstrated interesting behaviors. When cells were operated at lower currents, the gas evolution rates of the alkaline NaBH<sub>4</sub>-N<sub>2</sub>H<sub>4</sub> solutions were first decreased slightly and then increased linearly with increasing the current density. This result can be attributed to the competition between the hydrolysis reaction of BH<sub>4</sub><sup>-</sup>, electro-oxidation of H<sub>2</sub> and their anode reactions [6]. When operating cells at large currents, the gas evolution rates of the alkaline NaBH<sub>4</sub>-N<sub>2</sub>H<sub>4</sub> solutions showed certain linear relations but located between 4e reactions of NaBH<sub>4</sub> and N<sub>2</sub>H<sub>4</sub>. The gas evolution rate was decreased with increasing the N<sub>2</sub>H<sub>4</sub> portion in the alkaline NaBH<sub>4</sub>-N<sub>2</sub>H<sub>4</sub> solutions. These results implied that NaBH<sub>4</sub> and N<sub>2</sub>H<sub>4</sub> would be oxidized on different catalysts during operation.

In order to understand the reaction mechanism of the alkaline NaBH<sub>4</sub>–N<sub>2</sub>H<sub>4</sub> solutions on the composite catalyst, the gas evolution behaviors of the alkaline NaBH<sub>4</sub>–N<sub>2</sub>H<sub>4</sub> solutions on Pd, Ni and surface-treated Zr–Ni alloy were studied individually. Experimental results are shown in Figs. 2–4. It was found that gas evolution rates of the alkaline NaBH<sub>4</sub> solution and alkaline N<sub>2</sub>H<sub>4</sub> solution agreed with their stoichiometric relations of the 4e reaction on Pd, Ni and surface-treated alloy respectively. However, the gas evolution of the alkaline NaBH<sub>4</sub>–N<sub>2</sub>H<sub>4</sub> solutions on these electro-catalysts demonstrated different behaviors. The gas evolution behaviors of the alkaline NaBH<sub>4</sub>–N<sub>2</sub>H<sub>4</sub> solutions on Pd catalyst were close to that of alkaline NaBH<sub>4</sub> solution, which indicated that NaBH<sub>4</sub> would be mainly oxidized on Pd catalyst.

From our previous results, it was known that  $BH_4^-$  would be electro-oxidized on Ni or surface-treated Zr–Ni alloy through the 4e reaction [6,7]. However, the gas evolution behaviors of the alkaline NaBH<sub>4</sub>–N<sub>2</sub>H<sub>4</sub> solutions on Ni or surface-treated Zr–Ni alloy catalyst were close to that of alkaline N<sub>2</sub>H<sub>4</sub> solution, which implied that N<sub>2</sub>H<sub>4</sub> would be mainly oxidized on Ni or surface-treated Zr–Ni alloy catalyst when using alkaline NaBH<sub>4</sub>–N<sub>2</sub>H<sub>4</sub> solutions as the fuel.

Based on the results and discussion mentioned above, the decrease of gas evolution rate when using alkaline  $NaBH_4-N_2H_4$  solutions as the fuel, can be attributed to that  $N_2H_4$  would occupy some catalyst sites to be oxidized. As a result, less gas was generated during operation, due to that the anodic reaction of  $N_2H_4$ 



Fig. 3. Gas evolution rates of alkaline  $NaBH_4-N_2H_4$  solutions on the Ni catalyst. NaOH concentration: 10 wt.%.

generated less gas  $(1 \mod of N_2)$  compared with the anodic reaction of NaBH<sub>4</sub> (2 mol of H<sub>2</sub>).

It was noted that the gas evolution rate of the alkaline NaBH<sub>4</sub> solution at composite catalyst was lower than the stoichiometric relation of the 4e reaction of NaBH<sub>4</sub> according to Eq. (2). This implied that the generated electrons of the alkaline NaBH<sub>4</sub> solution on the composite catalyst were more than 4 electrons. However, the Ni and surface-treated Zr–Ni alloy gave a 4e H<sub>2</sub> stoichiometry except of Pd/C as shown in Figs. 2–4. It seems to be a discrepancy between Fig. 1 and Figs. 2–4.

Since the potential of  $BH_4^-$  at Ni catalyst was more negative than that of  $BH_4^-$  at Pd catalyst, it was considered that Ni was more active than Pd in borohydride solutions [7]. We supposed that borohydride reacted on Ni and surface-treated Zr–Ni alloy prior to Pd/C in the composite catalyst during operation, so that the actual concentration of borohydride on Pd/C surface in anode was decreased. It favored for improving the generated electrons of  $BH_4^-$  on Pd/C to be six or eight, which increased the coulumbic efficiency of  $BH_4^-$ . As a result, the gas evolution rate of the alkaline NaBH<sub>4</sub> solution at composite catalyst was lower than the stoichiometric relation of the 4e reaction of  $BH_4^-$ .



Fig. 4. Gas evolution rates of alkaline NaBH<sub>4</sub>–N<sub>2</sub>H<sub>4</sub> solutions on the surface-treated Zr–Ni alloy catalyst. NaOH concentration: 10 wt.%.



Fig. 5. Cyclic voltammograms of the alkaline NaBH<sub>4</sub>-N<sub>2</sub>H<sub>4</sub> solutions at a scan rate of 5 mV s<sup>-1</sup>. NaOH concentration: 10 wt.%.

#### 3.2. Cell performance

In order to understand more details about the electro-oxidation mechanism of the alkaline NaBH<sub>4</sub>–N<sub>2</sub>H<sub>4</sub> solutions, the cyclic voltammetry curves of the NaBH<sub>4</sub>–N<sub>2</sub>H<sub>4</sub> solutions were measured and shown in Fig. 5. The potential of NaBH<sub>4</sub> was more negative than that of N<sub>2</sub>H<sub>4</sub> at anodic maximum current. It indicated that both NaBH<sub>4</sub> and N<sub>2</sub>H<sub>4</sub> could be electro-oxidized in the alkaline NaBH<sub>4</sub>–N<sub>2</sub>H<sub>4</sub> solutions and BH<sub>4</sub><sup>-</sup> was more active than N<sub>2</sub>H<sub>4</sub>. It implied that BH<sub>4</sub><sup>-</sup> would be oxidized prior to N<sub>2</sub>H<sub>4</sub> when operating the DBFC using an alkaline NaBH<sub>4</sub>–N<sub>2</sub>H<sub>4</sub> solution as the fuel.

It was known that cell performance would be decreased when using high concentrated borohydride solutions as the fuel for the DBFC [18]. Here, we investigated the effect of  $N_2H_4$  replacement for NaBH<sub>4</sub> on the cell performance. Fig. 6 shows the cell performances when using alkaline NaBH<sub>4</sub>–N<sub>2</sub>H<sub>4</sub> solutions as the fuel. It was found that N<sub>2</sub>H<sub>4</sub> addition in alkaline NaBH<sub>4</sub> solution would not influence the open-circuit voltage (OCV) of the DBFC. The OCVs of the DBFC using alkaline NaBH<sub>4</sub>–N<sub>2</sub>H<sub>4</sub> solutions were higher than that of the DHFC, but there was no significant differ-



**Fig. 6.** Cell performances when using alkaline NaBH<sub>4</sub>-N<sub>2</sub>H<sub>4</sub> solutions as the fuel. NaOH concentration: 10 wt.%.

ence between the performance of DHFC and DBFC using alkaline NaBH<sub>4</sub>–N<sub>2</sub>H<sub>4</sub> solutions. For the DBFC, N<sub>2</sub>H<sub>4</sub> addition in alkaline NaBH<sub>4</sub> solution improved the cell performance. A maximum power density of  $64 \text{ mW cm}^{-2}$  has been achieved when using the alkaline NaBH<sub>4</sub>–N<sub>2</sub>H<sub>4</sub> solution containing 5 wt.% of NaBH<sub>4</sub>, 10 wt.% of N<sub>2</sub>H<sub>4</sub> and 10 wt.% of NaOH. It may be attributed to that the depression of gas evolution decreased the cell resistance during operation [20]. For the DHFC, adding sodium borohydride into alkaline hydrazine solutions can improve fuel capacity because the capacity of NaBH<sub>4</sub> (5.67 Ah g<sup>-1</sup>) is higher than that of N<sub>2</sub>H<sub>4</sub> (3.35 Ah g<sup>-1</sup>).

It is known that  $N_2H_5^+$  would be formed due to  $N_2H_4$  hydrolysis [21]. It is considered that an ion complex of  $N_2H_5^+$ ·BH<sub>4</sub><sup>-</sup> would be formed in the alkaline NaBH<sub>4</sub>–N<sub>2</sub>H<sub>4</sub> solutions so that the crossover of  $N_2H_5^+$  ions would be suppressed. As a result, OCVs of the DBFC using alkaline NaBH<sub>4</sub>–N<sub>2</sub>H<sub>4</sub> solutions were higher than that of the DHFC using alkaline hydrazine solution as the fuel. More efforts should be made to prove the existence of the  $N_2H_5^+$ ·BH<sub>4</sub><sup>-</sup> ion complex.

#### 4. Conclusions

The addition of  $N_2H_4$  in alkaline borohydride solutions can suppress the gas evolution of the DBFC during operation. NaBH<sub>4</sub> would be mainly oxidized on Pd whereas  $N_2H_4$  would be mainly oxidized on Ni or surface-treated Zr–Ni alloy catalyst when using alkaline NaBH<sub>4</sub>– $N_2H_4$  solutions as the fuel and a composite of Pd, Ni and surface-treated Zr–Ni alloy as the anodic catalyst.

The DBFC performance was improved by adding  $N_2H_4$  into the alkaline NaBH<sub>4</sub> solutions and its performance was comparable to that of DHFC in this study. A maximum power density of  $64 \,\mathrm{mW}\,\mathrm{cm}^{-2}$  was achieved when operating the cell at ambient conditions. The alkaline NaBH<sub>4</sub>-N<sub>2</sub>H<sub>4</sub> solution is suitable for both DBFC and DHFC.

#### Acknowledgements

This work is financially supported by Hi-tech R&D Program of China (863), grant no. 2006AA05Z120 and 2007AA05Z144, Doctoral Fund from Education Ministry of China (20070335003) as well as Fund from Science & Technology Ministry of Zhejiang Province (2007R10029).

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